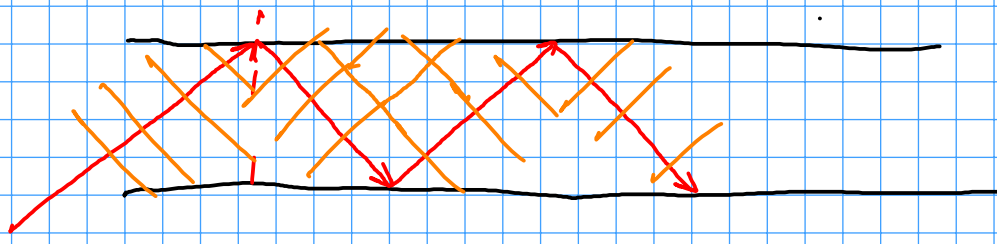
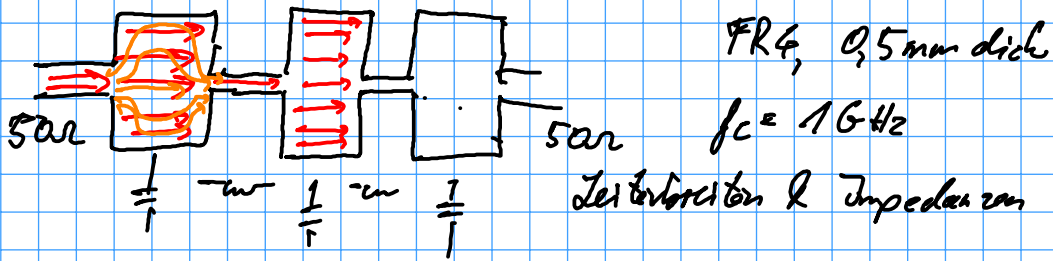


geschlossen  
nur geschlossen



# Entwurf TP-Filter mit Leitungsstücken



$50 \Omega$   $w = 1 \text{ mm}$  ;  $D_{50} = 171 \text{ mm}$

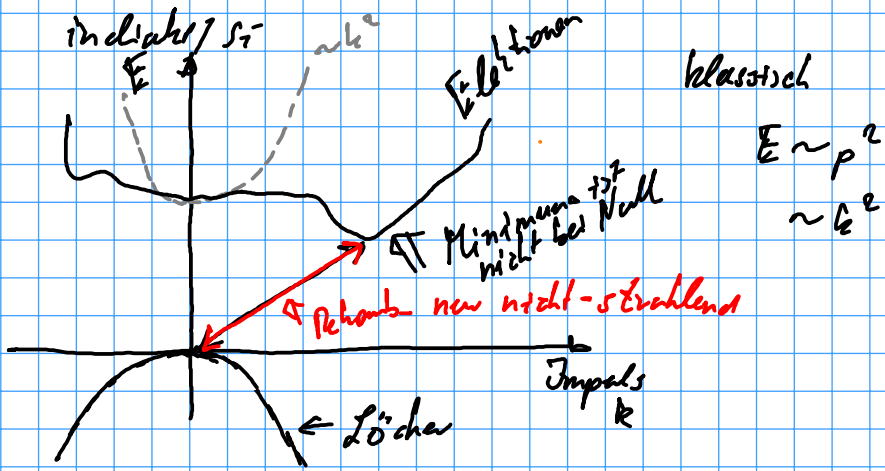
$99 \Omega$  ( $100 \Omega$ )  $w_H = 0,25 \text{ mm}$   $D_H = 180 \text{ mm}$   $Z_H = 100 \Omega$

$15 \Omega$   $w_L = 5 \text{ mm}$   $D_L = 160 \text{ mm}$   $Z_L = 15 \Omega$

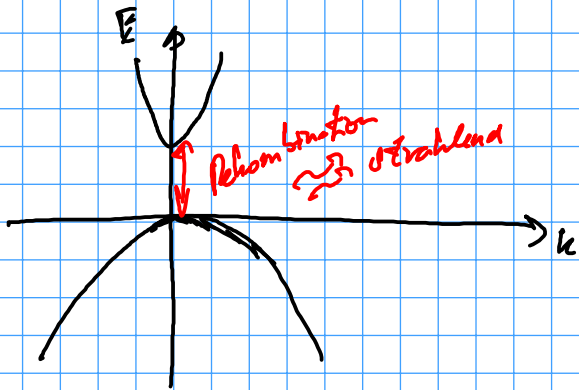
Wähle Tschubyscheff-Filter mit  $\alpha_{0.05} = 1 \text{ dB}$   $N = 5$

$K$	Coax $L$	$l$
2,135	6,8 pF	17,7 mm
1,097	8,68 nH	16,5 mm
3,007	3,55 pF	28,5 mm

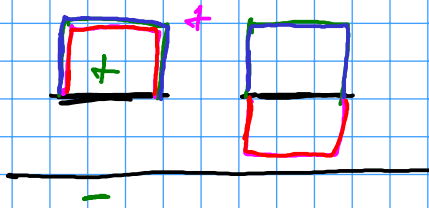
# Halbleiter



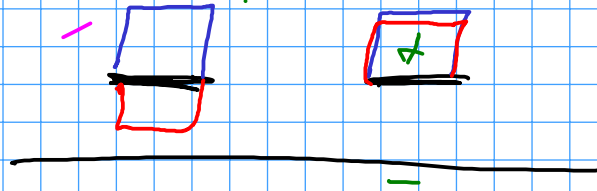
direkt / VL / GaAs



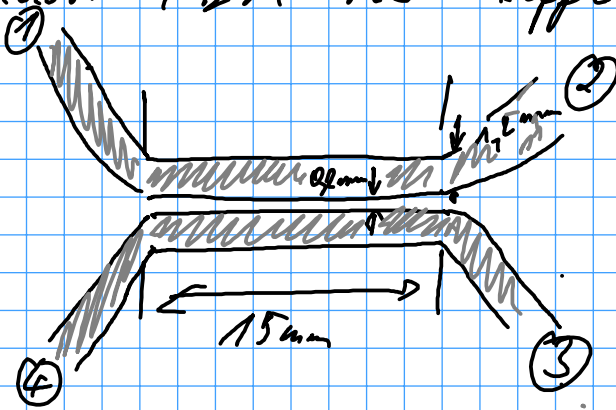
# Gleich- & Gegenlaufwelle



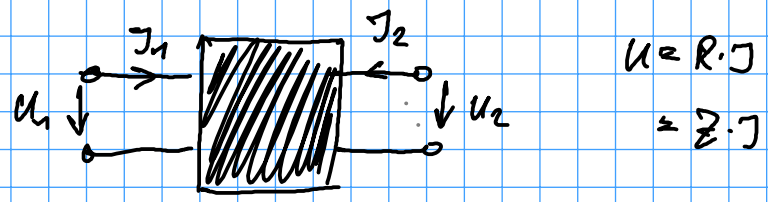
nach etwas Distanz und  
rot hat andere Geschwindigkeit/  
Wellenlänge als blau



# Quasi-TEM-MS-Koppler



# 4 Pol bzw. 2-Port Parameter

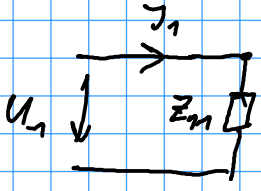


$$U = R \cdot J$$
$$= Z \cdot J$$

$$\begin{pmatrix} U_1 \\ U_2 \end{pmatrix} = \begin{pmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{pmatrix} \begin{pmatrix} J_1 \\ J_2 \end{pmatrix}$$

Annahme:  $J_2 = 0$  (Leerlauf rechts) &  $J_1$  eingespeist

$$U_1 = Z_{11} \cdot J_1 \quad ; \quad U_2 = Z_{21} \cdot J_1$$

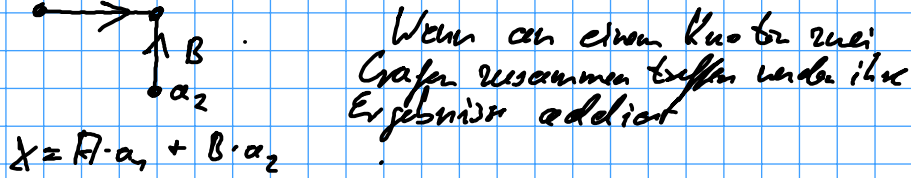
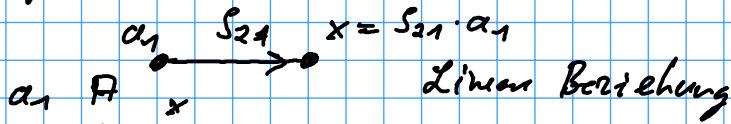


geht auch anders herman

# Signalflussgraphen

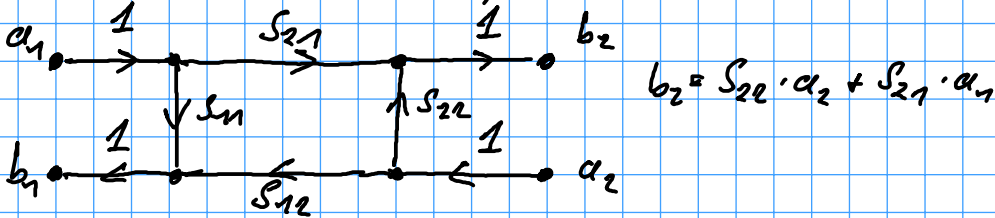
Knoten  $\bullet$  hat Wert bspw.  $a_1$  oder  $a_2$  ...

Grafen  $\xrightarrow{S_{21}}$  hat auch Wert bspw.  $S_{21}$



$\Rightarrow$  Damit hat man die Möglichkeit sämtliche lineare Beziehungen auszudrücken.

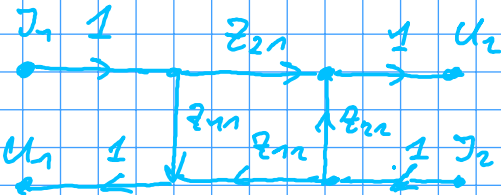
$$\begin{pmatrix} b_1 \\ b_2 \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix}$$



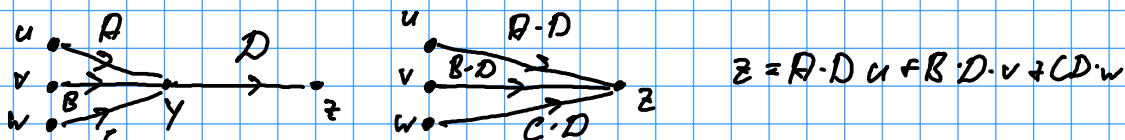
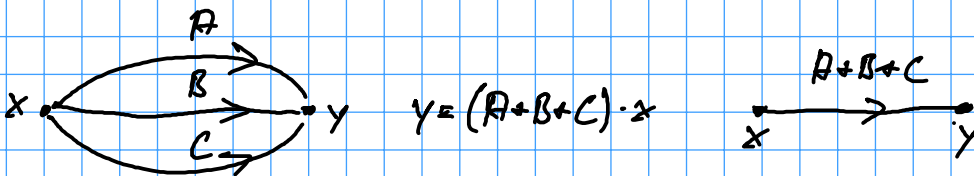
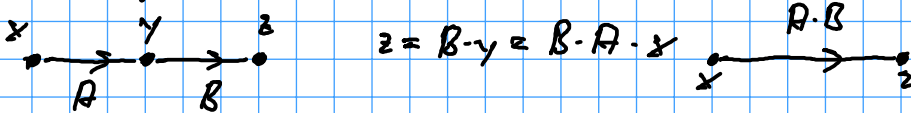
$$b_1 = S_{11} \cdot a_1 + S_{12} \cdot a_2$$

Bei 2-Parametern 4-Pol

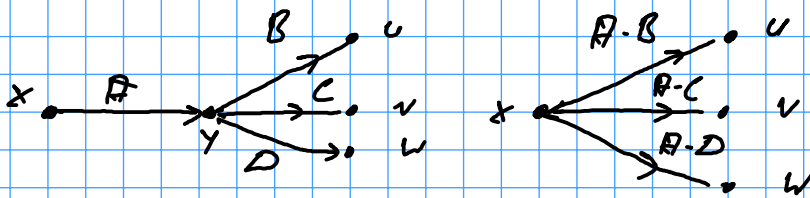
$$\begin{pmatrix} U_1 \\ U_2 \end{pmatrix} = \begin{pmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{pmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$



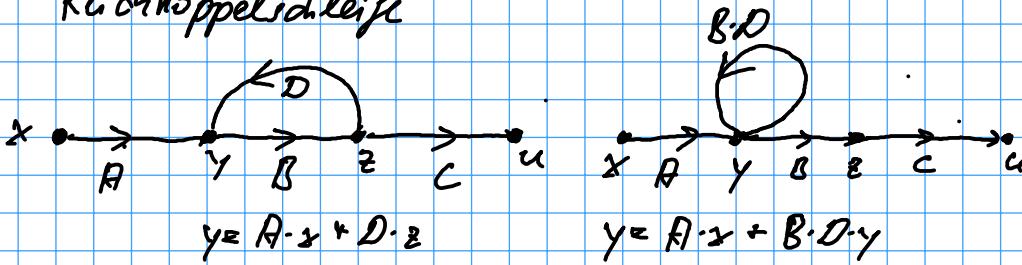
Rechenregeln



Knoten y wurde aufgespalten und ist damit zerstört worden.

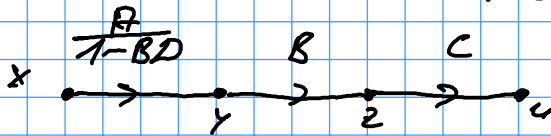


### Rückkopplungsschleife

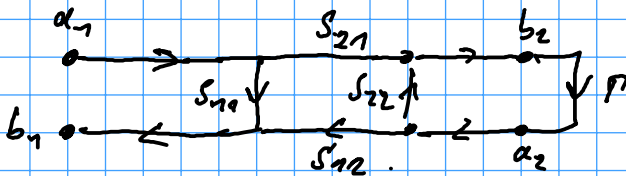
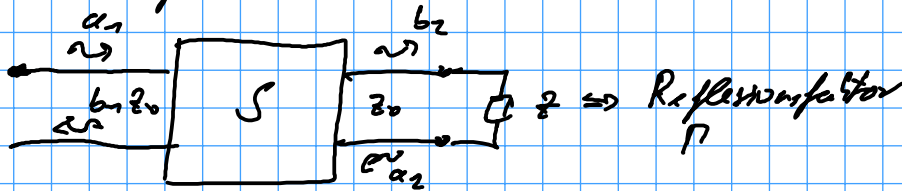


$$\Leftrightarrow y \cdot (1 - BD) = A \cdot x$$

$$\Leftrightarrow y = \frac{A}{1 - BD} \cdot x$$



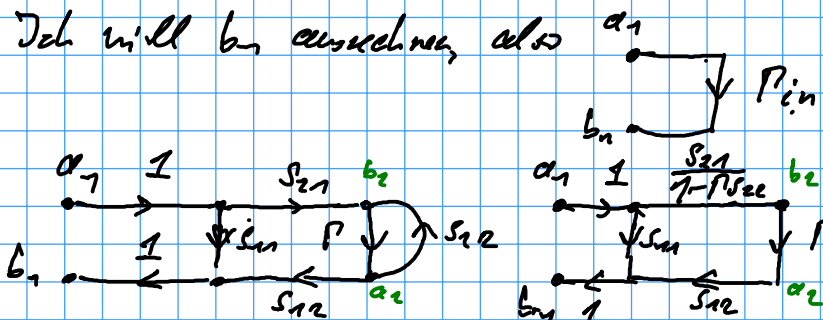
### Praktisch für 6-Port



$$\begin{pmatrix} b_1 \\ b_2 \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix} \quad \text{und } a_2 = P \cdot b_2$$

$a_1$  gegeben

Ich will  $b_1$  ausrechnen, also



$$b_1 = S_{11} \cdot a_1 + \frac{S_{21} \cdot P \cdot S_{12}}{1 - P \cdot S_{22}} \cdot a_1$$

$$= \underbrace{\left( S_{11} + \frac{S_{21} \cdot P \cdot S_{12}}{1 - P \cdot S_{22}} \right)}_{P_{in}} \cdot a_1$$

$$P=0 : b_1 = S_{11} \cdot \alpha_1$$

$$S_{21} = 0 \quad b_1 = (S_{11} + S_{21} P \cdot S_{12}) \alpha_1 \quad \text{keine Rückkopplung}$$

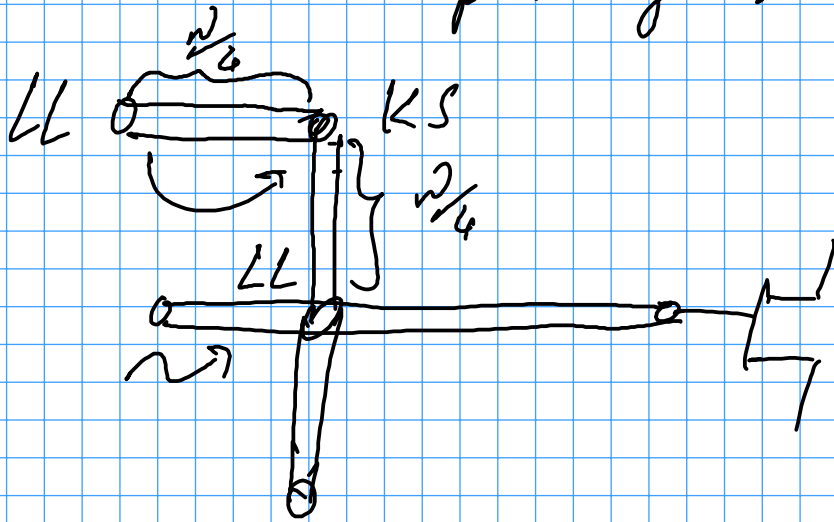
$$S_{21} \approx 1, P \approx 1 \quad b_1 = \left( S_{11} + \frac{S_{21} P S_{12}}{\text{was kleines}} \right) \alpha_1 \quad \uparrow$$

Wie groß ist  $b_2$ ?

$$\text{hier ist } b_2 = \frac{S_{21}}{1 - P S_{22}} \cdot \alpha_1 \quad \text{Aber in Anwesenheit  
keine nur über } \alpha_1$$



# Verspannungs-NW mit Leitung



20 92 GHz

## Verstärker

$$f = 1250 \text{ MHz}$$

entweder mit BFP 450  $\rightarrow$  low-noise

BFU 590  $\rightarrow$  mittel Leistung